

SUBSIDENCE IN THREE DIMENSIONS: CENTER OF DILATION (MOGI SOURCE) (43)

I Main Topics

A Center of dilation (contraction) in a half-space

B Case histories

C References

* Patterned after Segall, 2010

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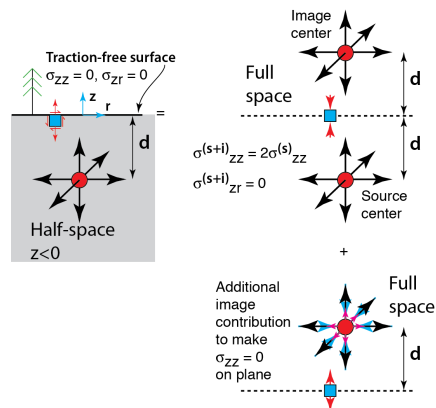
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II Center of dilation in half-space (Mogi source)

A Construction of solution by sources and images

- 1 Half-space: $z < 0$
- 2 Source center in a full space, *by itself*, has local radial displacements and stress singularity, but induces stresses along midplane (dashed) between source and image
- 3 Image center has strength of source, but is located above midplane
- 4 Source and image together double σ_{zz} along midplane; annul σ_{zr}
- 5 Additional image contribution annulls σ_{zz} along midplane between source and image

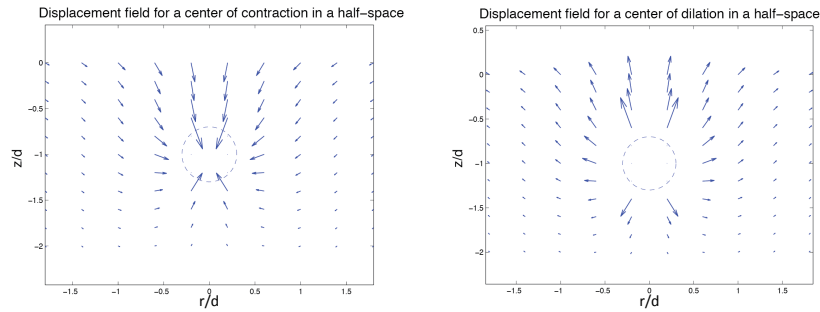


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B Sub-surface displacement field ($z < 0$) for centers of contraction and dilation



- 1 Displacements (and hence strains) near center similar to those for a center in an infinite body
- 2 Displacements at the surface radiate towards or from center at depth (just like for a center in an infinite body) but are larger by a factor of $4(1-\nu)$ [Davies, 2003]

C Displacement field at the surface ($z = 0$) for a center of dilation

Center of contraction
Infinite linear elastic body

Displacements are radial (towards center) everywhere, including near center

Center of contraction
Linear elastic half-space

Purely radial displacements (towards center) along surface and near center

Displacements at the surface of half-space radiate towards or from center at depth (just like for a center in an infinite body) but are larger by a factor of $4(1-\nu)$ [Davies, 2003]

$u_R^\infty = \frac{\Delta V}{4\pi} \frac{R}{R^3}$

At plane a distance d above center

$u_{R(z=0)}^\infty = \frac{\Delta V}{4\pi} \frac{(r^2 + d^2)^{1/2}}{R^3}$

$u_{r(z=0)}^\infty = \frac{\Delta V}{4\pi} \frac{r}{R^3}$

$u_{z(z=0)}^\infty = \frac{\Delta V}{4\pi} \frac{d}{R^3}$

At surface ($z=0$)

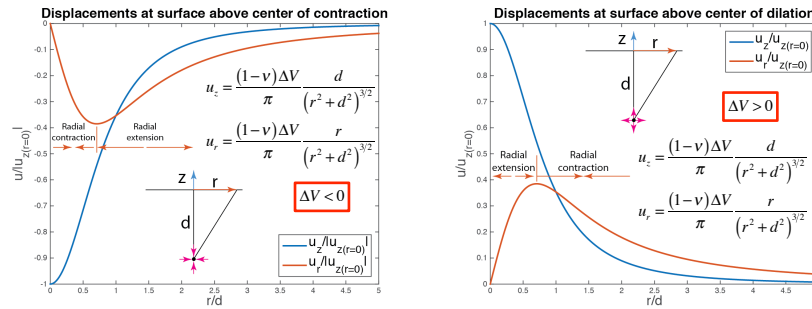
$u_{R(z=0)}^{hs} = (1-\nu) \frac{\Delta V}{\pi} \frac{R}{R^3}$

$u_{R(z=0)}^{hs} = (1-\nu) \frac{\Delta V}{\pi} \frac{(r^2 + d^2)^{1/2}}{R^3} = [4(1-\nu)] u_{R(z=0)}^\infty$

$u_{r(z=0)}^{hs} = (1-\nu) \frac{\Delta V}{\pi} \frac{r}{R^3} = [4(1-\nu)] u_{r(z=0)}^\infty$

$u_{z(z=0)}^{hs} = (1-\nu) \frac{\Delta V}{\pi} \frac{d}{R^3} = [4(1-\nu)] u_{z(z=0)}^\infty$

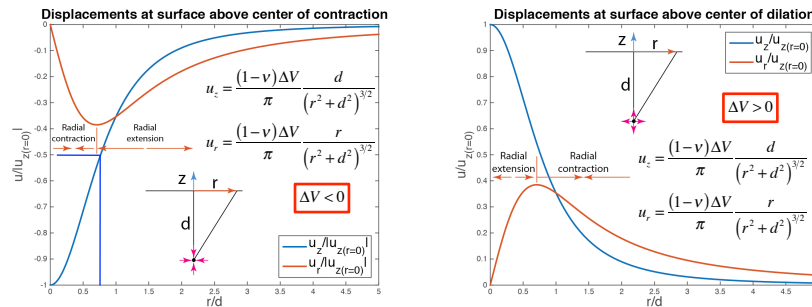
D Displacements at the surface (z = 0) for centers of contraction and dilation



Radial strain ϵ_{rr} at $z = 0$	Center of contraction	Center of dilation
$r/d < 0.71$	Contraction	Extension
$r/d > 0.71$	Extension	Contraction

Vertical displacement magnitude decrease by 50% at $r_{1/2} \approx 0.77d$

E Displacements at the surface (z = 0) for centers of contraction and dilation



Vertical displacement magnitude decreases by 50% at $r_{1/2} \approx 0.77d$

So, $d \approx r_{1/2}/0.77$

The maximum radial displacement occurs at $r^* \approx 0.71d$

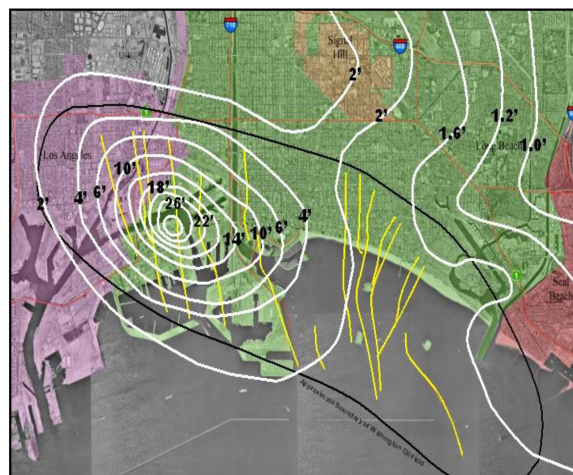
So, alternatively, $d \approx r^*/0.71$

From d and ground displacements at different positions, ΔV can be calculated

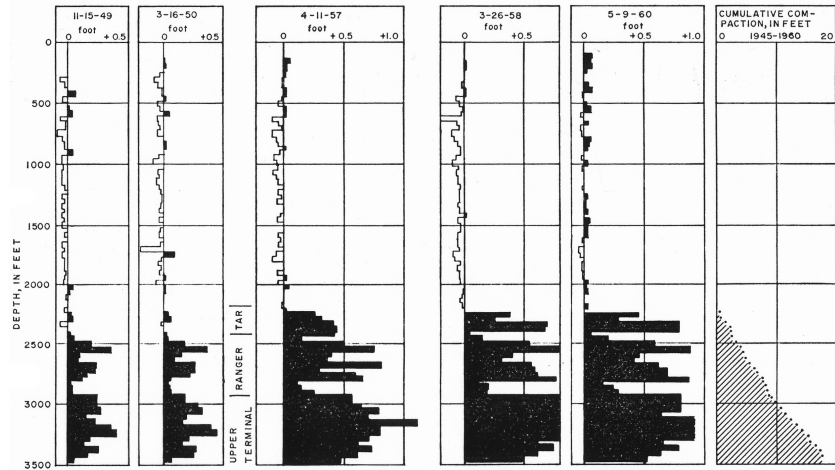
III Case histories

- 1 Wilmington oil field, Long Beach, CA
- 2 Darwin volcano, Galapagos Islands

1 Surface displacements, Wilmington oil field, Long Beach, CA



A Vertical extension above producing horizons



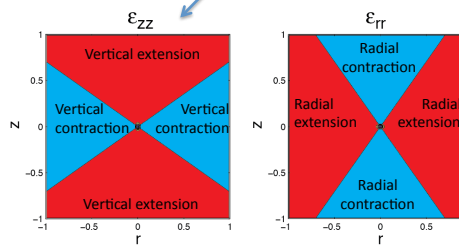
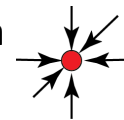
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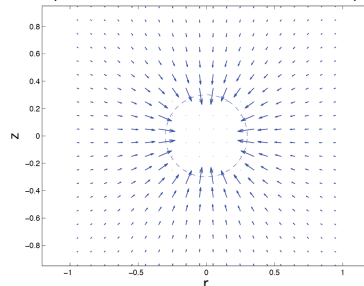
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B Normal strains and displacements in a vertical plane through a center of contraction

Vertical extension predicted above producing horizons



Displacement field for a center of dilation in full space



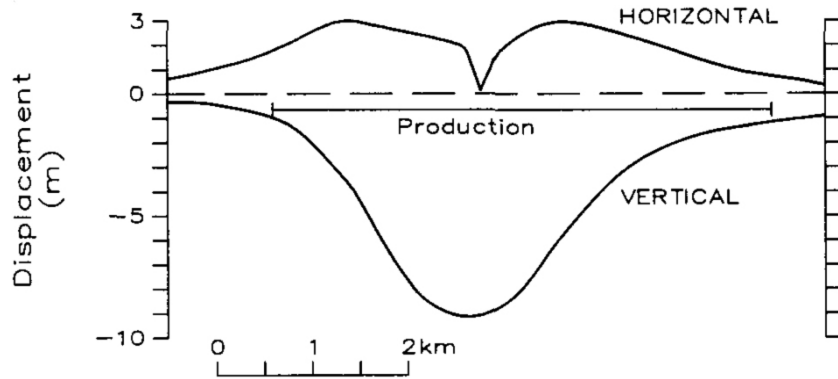
Displacements not shown within dashed circle for diagrammatic reasons

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C Surface displacements from the Wilmington oil field, Long Beach, CA

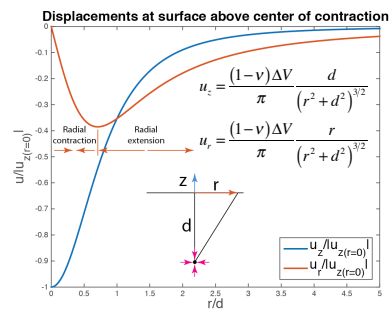
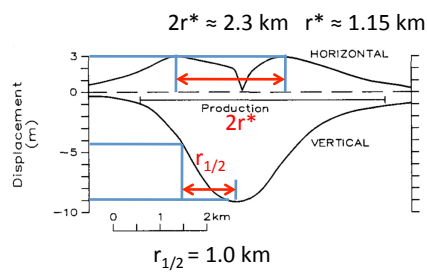


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D Wilmington oil field data and model predictions



$$d \approx r_{1/2} / 0.77 = 1.0 \text{ km} / 0.77 = 1.3 \text{ km}$$

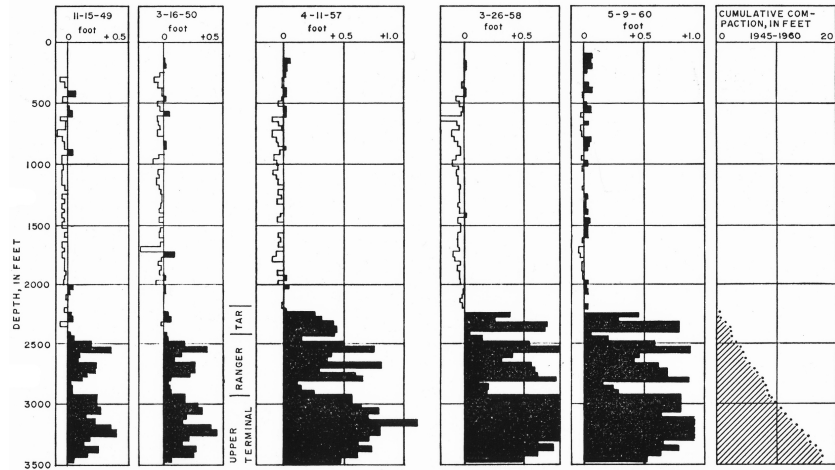
$$d \approx r^* / 0.71 = 1.15 \text{ km} / 0.71 = 1.5 \text{ km}$$

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E Producing horizons centered at ~ 1km depth

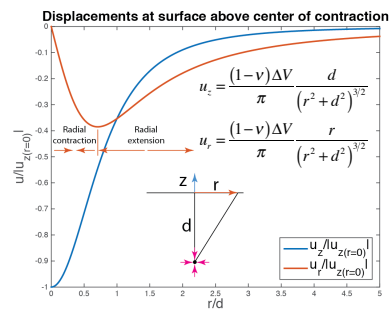
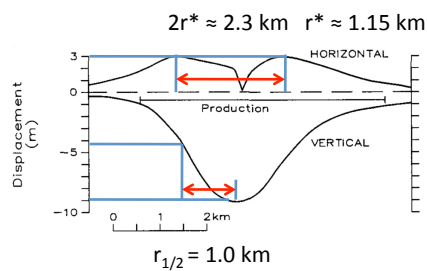


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F Wilmington oil field data and model predictions for volume loss



$$d \approx r_{1/2} / 0.77 = 1.0 \text{ km} / 0.77 = 1.3 \text{ km}$$

$$d \approx r^* / 0.71 = 1.15 \text{ km} / 0.71 = 1.5 \text{ km}$$

$$\Delta V = \frac{u_z \pi}{(1-\nu)} \frac{[r^2 + d^2]^{3/2}}{d} = \frac{(-9m) \pi ((0m)^2 + (1300m)^2)^{3/2}}{(1-0.25) 1300m} = -6.4 \times 10^7 m^3$$

$$\Delta V = \frac{u_r \pi}{(1-\nu)} \frac{[r^2 + d^2]^{3/2}}{r} = \frac{(-3m) \pi ((1150m)^2 + (1500m)^2)^{3/2}}{(1-0.25) 1500m} = -7.4 \times 10^7 m^3$$

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G Produced volume at Wilmington oil field vs. model predictions

From November 1936 to July 1, 1969 the oil field produced approximately 2.0×10^8 cubic meters (Mayuga and Allen)

$$\Delta V = \frac{u_r \pi [r^2 + d^2]^{3/2}}{(1-\nu) d} = \frac{(-9m) \pi ((0m)^2 + (1300m)^2)^{3/2}}{(1-0.25) 1300m} = -6.4 \times 10^7 m^3$$

$$\Delta V = \frac{u_r \pi [r^2 + d^2]^{3/2}}{(1-\nu) r} = \frac{(-3m) \pi ((1150m)^2 + (1500m)^2)^{3/2}}{(1-0.25) 1500m} = -7.4 \times 10^7 m^3$$

Fluid volume produced is ~ 3 times the modeled solid volume loss

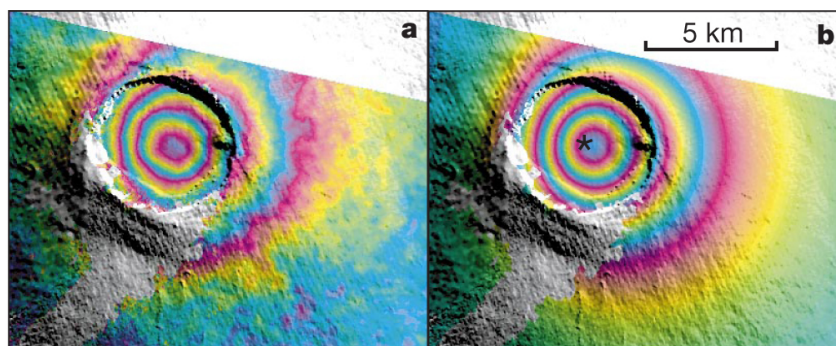
Possible parallel: in the San Joaquin Valley, the pumped volume is ~ 3 times the subsidence volume

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2 Darwin volcano: ground surface displacements vs. model predictions



SAR interferogram of Darwin volcano, Galapagos Islands. (a) Data from 1992 to 1998. (b) Predicted interferogram based on a center of dilation located at a depth of 3 km beneath the star. Each color cycle represents 5 cm of displacement along the line of sight. From Amelung et al., 2000.

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References

- Amelung, F., S. Jonsson, H. Zebker and P. Segall, 2000, Widespread uplift and trap door faulting on Galápagos volcanoes observed with radar interferometry: *Nature*, v. 407, p. 993-996.
- Davies, J.H., 2003, Elastic field in a semi-infinite solid due to thermal expansion or a coherently misfitting inclusion: *Journal of Applied Mechanics*, v. 70, p. 655-660.
- Geertsma, J., 1973, Land subsidence above compacting oil and gas reservoirs: *Journal of Petroleum Technology*, v. 25, p. 734-744.
- Mayuga, M.N., and Allen, D.R., date unknown, Subsidence in the Wilmington oil field, Long Beach, California, U.S.A., p. 66-79, <http://www.saveballona.org/gasoilfields/WilmSubGC.pdf>.
- McTigue, D.F., 1987, Elastic stress and deformation near a finite spherical magma body: resolution of the point source paradox: *Journal of Geophysical Research*, v. 92, p. 12,931-12,940.
- Mindlin, R.D., 1936, Force at a point in the interior of a semi-infinite solid: *Physics*, v. 7, p. 195-206.
- Mindlin, R. D., and Cheng, D. H., 1950, "Nuclei of strain in the semi-infinite solid," *Journal of Applied Physics*, v.21, p. 926-930.
- Mogi, K., 1958, Relations between the eruptions of various volcanoes and the deformations of the ground surfaces around them, *Bulletin of the Earthquake Research Institute*, v. 36, p. 99-134.
- Segall, P., 1989, Earthquakes Triggered by Fluid Extraction: *Geology*, v. 17, p. 942-946.
- Segall, P., 2010, *Earthquake and volcano deformation: Princeton University Press, Princeton, New Jersey, 432 p.*
- Wang, H., 2000, *Theory of linear poroelasticity: Princeton University Press, Princeton, New Jersey, 287 p.*