11/5/02

CAUCHY'S FORMULA AND EIGENVAULES (PRINCIPAL STRESSES) IN 3-D

- I Main Topics
 - A Cauchy's formula
 - B Principal stresses (eigenvectors and eigenvalues)
- II Cauchy's formula
 - A Relates traction vector components to stress tensor components (see Figures 19.1, 19.2, 19.3 for derivation)
 - B $\tau_i = \sigma_{ji} n_j$
 - 1 Meaning of terms
 - a τ_i =traction vector component: $\vec{\tau} = \tau_1 \vec{i} + \tau_2 \vec{j} + \tau_3 \vec{k}$
 - b σ_{ij} = stress component
 - c n =unit normal. The components n_j of the unit normal are the direction cosines between n and the coordinate axes.

d
$$\frac{F_i}{A} = \frac{F_i}{A_1} \frac{A_1}{A} + \frac{F_i}{A_2} \frac{A_2}{A} + \frac{F_i}{A_3} \frac{A_3}{A}$$

- 2 This represents the physics directly
- 3 The traction component that acts *in* the i-direction reflects the contribution of the stresses that act *in* that direction.
- 4 Note that the j's "cancel out" in equation II.B
- 5 Note that the subscripts on the τ and the n differ
- 6 σ is symmetric ($\sigma_{ij} = \sigma_{ji}$), so ...
- C $\tau_i = \sigma_{ij} n_j$ Standard form of Cauchy's formula
 - 1 The subscript j's still "cancel out"
 - 2 The subscripts on the τ and the n still differ
 - 3 Easier(?) to remember than "B"
- D Full expansion

 $\tau_i = \sigma_{ji} n_j$ $\tau_i = \sigma_{ij} n_j$ $\tau_1 = \sigma_{11} n_1 + \sigma_{21} n_2 + \sigma_{31} n_3$ $= \sigma_{11} n_1 + \sigma_{12} n_2 + \sigma_{13} n_3$ $\tau_2 = \sigma_{12} n_1 + \sigma_{22} n_2 + \sigma_{32} n_3$ $= \sigma_{21} n_1 + \sigma_{22} n_2 + \sigma_{23} n_3$ $\tau_3 = \sigma_{13} n_1 + \sigma_{23} n_2 + \sigma_{33} n_3$ $= \sigma_{31} n_1 + \sigma_{32} n_2 + \sigma_{33} n_3$ Matrix form

 $\begin{bmatrix} \tau_1 \\ \sigma_{11} & \sigma_{21} & \sigma_{23} \end{bmatrix} \begin{bmatrix} n_1 \\ n_2 \end{bmatrix} = \begin{bmatrix} \sigma_{12} & \sigma_{22} & \sigma_{32} \end{bmatrix} \begin{bmatrix} n_2 \\ n_2 \end{bmatrix}$ $\begin{bmatrix} \tau_1 \\ \sigma_{13} & \sigma_{23} & \sigma_{33} \end{bmatrix} \begin{bmatrix} n_2 \\ \sigma_{13} & \sigma_{23} & \sigma_{33} \end{bmatrix} \begin{bmatrix} n_3 \end{bmatrix}$ $\begin{bmatrix} \tau_1 \\ \sigma_{11} & \sigma_{12} & \sigma_{13} \end{bmatrix} \begin{bmatrix} \tau_1 \\ \sigma_{12} & \sigma_{13} & \sigma_{23} & \sigma_{33} \end{bmatrix} \begin{bmatrix} n_2 \\ \sigma_{13} & \sigma_{23} & \sigma_{33} \end{bmatrix} \begin{bmatrix} n_3 \end{bmatrix}$

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 $\Sigma \mathbf{F}_1 = 0$, so $(\Sigma \mathbf{F}_1)/\mathbf{A} = 0$.

 $\tau_1(A/A) = (\sigma_{11})(A_1/A) + (\sigma_{21})(A_2/A).$

Similarly, $(\Sigma F_2)/A = 0$, so

$$\tau_2(\mathsf{A}/\mathsf{A}) = (\sigma_{12})(\mathsf{A}_1/\mathsf{A}) + (\sigma_{22})(\mathsf{A}_2/\mathsf{A}).$$



The ratio of the areas is given by the direction cosines of the normal to plane A. This holds in 2-D and in 3-D also.

Substituting for the area ratios:

$$\begin{aligned} &\tau_1 = (\sigma_{11})(n_1) + (\sigma_{21})(n_2). \\ &\tau_2 = (\sigma_{12})(n_1) + (\sigma_{22})(n_2). \\ &\tau_i = \sigma_{ji} \ n_j \end{aligned}$$

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19.0



$$\begin{split} \Sigma \mathbf{F}_1 &= 0, \text{ so } (\Sigma \mathbf{F}_1) / A = 0. \\ \tau_1(A/A) &= (\sigma_{11})(A_1/A) + (\sigma_{21})(A_2/A) + (\sigma_{31})(A_3/A). \\ \text{Similarly, } \Sigma \mathbf{F}_2 &= 0 \text{ and } \Sigma \mathbf{F}_3 = 0, \text{ so} \\ \tau_2(A/A) &= (\sigma_{12})(A_1/A) + (\sigma_{22})(A_2/A) + (\sigma_{32})(A_3/A). \\ \tau_3(A/A) &= (\sigma_{13})(A_1/A) + (\sigma_{23})(A_2/A) + (\sigma_{33})(A_3/A). \end{split}$$

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Note that Δ DCB of area A projects onto the x_1 - x_2 plane as Δ OCB, onto the x_2 - x_3 plane as Δ OCD, and onto the x_3 - x_1 plane as Δ OBD.

BOP⁺ is perpendicular to CD, and because CD is a line in BCD, BOP' is perpendicular to BCD. Similarly, COP" is perpendicular to BD, so COP" is perpendicular to BCD. The intersection of BOP' and COP' is perpendicular to BCD, and that intersection is OP.

 $\omega_1, \omega_2, \omega_3$, are angles between OP and x_1, x_2 , and x_3 , respectively.

A ₁ =	= 1/2 (base OCD)(height OCD) =	= (CD)(OP') =	= OP'
A	1/2 (base DCB)(height CBD)	(CD)(BP')	BP'



$$\tau_3 = (\sigma_{13})(n_1) + (\sigma_{23})(n_2) + (\sigma_{33})(n_3).$$

So $\tau_i = \sigma_{ji} n_{j}$, but $\sigma_{ij} = \sigma_{ji}$, so $\tau_i = \sigma_{ij} n_j$

III Principal stresses from tensor and matrix perspectives

Consider a plane with a normal vector **n** defined by direction cosines n₁, n₂, and n₃. The components of traction τ on the plane, by Cauchy's formula, are $\tau_i = \sigma_{ij} n_j$. They also are simply the components of $\tau: \tau_1 = \tau n_1$, $\tau_2 = \tau n_2$, and $\tau_3 = \tau n_3$. The components can be equated:

(1)
$$\begin{bmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{bmatrix} \begin{bmatrix} n_1 \\ n_2 \\ n_3 \end{bmatrix} = T \begin{bmatrix} n_1 \\ n_2 \\ n_3 \end{bmatrix}.$$

The right side of (1) can be subtracted from the left side to yield:

(2)
$$\begin{bmatrix} \sigma_{11} - T & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} - T & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} - T \end{bmatrix} \begin{bmatrix} n_1 \\ n_2 \\ n_3 \end{bmatrix} = 0.$$

Equation (2) can be rewritten

(3)
$$[\sigma - I T] [n] = 0$$
, where I is the identity matrix
(4) $I = \begin{vmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{vmatrix}$. For any square matrix [A], [A][I] = [A].

According to theorems of linear algebra, equation (2) can be solved only if the determinant $I\sigma$ -ITl equals zero:

(5)
$$\begin{vmatrix} \sigma_{11} - T & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} - T & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} - T \end{vmatrix} = 0$$

In many cases the components of σ are known but T is must be solved for. Problems of the form of equation (3) are common in many branches of mathematics, engineering, and physics, and they have a special name: eigenvalue problems. The values of T (i.e., **ITI**, the principal values) that solve the equation <u>are called eigenvalues</u>, and the vectors **n** (the principal <u>directions</u>) that give the directions of **T** <u>are called eigenvectors</u>. Because these problems are so common, many mathematics packages, including Matlab, have special routines to solve for eigenvalues and eigenvectors. Solving (5) by hand requires finding the roots of a cubic equation (not easy), so we consider the easier 2-D case, which yields a quadratic equation.

(6)
$$\begin{vmatrix} \sigma_{11} - T & \sigma_{12} \\ \sigma_{21} & \sigma_{22} - T \end{vmatrix} = 0$$
 Note: $\begin{vmatrix} a & b \\ c & d \end{vmatrix} = ad - bc$

(7)
$$(\sigma_{11} - T)(\sigma_{22} - T) - (\sigma_{12})(\sigma_{21}) = 0$$

(8)
$$T^2 - T(\sigma_{11} + \sigma_{22}) + (\sigma_{11})(\sigma_{22}) - (\sigma_{12})(\sigma_{21}) = 0$$

(9a)
$$T^2 - T(\sigma_{11} + \sigma_{22}) + [(\sigma_{11})(\sigma_{22}) - (\sigma_{12})^2] = 0$$
 or (9b) $T^2 - T(I_1) + [T_2] = 0$

The term T in equation (9) is solved using the quadratic formula: (10) $T = \frac{(\sigma_{11} + \sigma_{22}) \pm \sqrt{(\sigma_{11} + \sigma_{22})^2 - 4[(\sigma_{11})(\sigma_{22}) - (\sigma_{12}^2)]}}{2} = \frac{I_1 \pm \sqrt{I_1^2 - 4I_2}}{2}$

(11)
$$T = \frac{(\sigma_{11} + \sigma_{22}) \pm \sqrt{(\sigma_{11}^2 + 2\sigma_{11}\sigma_{22} + \sigma_{22}^2) - 4[(\sigma_{11})(\sigma_{22}) - (\sigma_{12}^2)]}}{2}$$

(12)
$$T = \frac{(\sigma_{11} + \sigma_{22}) \pm \sqrt{(\sigma_{11}^2 - 2\sigma_{11}\sigma_{22} + \sigma_{22}^2) + 4[\sigma_{12}^2]}}{2}$$

(13)
$$T = \frac{(\sigma_{11} + \sigma_{22}) \pm \sqrt{(\sigma_{11} - \sigma_{22})^2 + 4[\sigma_{12}^2]}}{2} = \frac{I_1 \pm \sqrt{I_1^2 - 4I_2}}{2}$$

(14)
$$T = \left[\frac{\sigma_{11} + \sigma_{22}}{2}\right] \pm \left[\sqrt{\left(\frac{\sigma_{11} - \sigma_{22}}{2}\right)^2 + \sigma_{12}^2}\right] = [c] \pm [r] = \left[\frac{I_1}{2}\right] \pm \left[\sqrt{\left(\frac{I_1}{2}\right)^2 - I_2}\right] = \sigma_1, \sigma_2$$

An inspection of the diagram below shows that the first term in brackets in equation (14) is the mean normal stress (i.e., the center of the Mohr circle) and the second term in brackets is the maximum possible shear stress (i.e., the radius of the Mohr circle). So the principal stresses lie at the end of a horizontal diameter through the Mohr circle. The terms $c, r, I_i, and I_2$ are called invariants and are independent of the frame of reference.



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Example Suppose the stress state at a point is given by (15) $\sigma_{ij} = \begin{bmatrix} 10 & 3 \\ 3 & 2 \end{bmatrix}$, where dimensions are in MPa. Solving for the principal values using eq. (14) yields (16) $\lambda = \frac{(10+2)}{2} \pm \sqrt{\left(\frac{10-2}{2}\right)^2 + 3^2} = 6 \pm \sqrt{25} = 11 \text{ and } 1$ Now we substitute these back into (3) (17a) $\begin{bmatrix} 10-11 & 3 \\ 3 & 2-11 \end{bmatrix} \begin{bmatrix} n_1 \\ n_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \implies \begin{bmatrix} -1 & 3 \\ 3 & -9 \end{bmatrix} \begin{bmatrix} n_1 \\ n_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$ for $T = \sigma_1 = 11$ MPa. (17b) $\begin{bmatrix} 10-1 & 3 \\ 3 & 2-1 \end{bmatrix} \begin{bmatrix} n_1 \\ n_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \implies \begin{bmatrix} 9 & 3 \\ 3 & 1 \end{bmatrix} \begin{bmatrix} n_1 \\ n_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$ for $T = \sigma_2 = 1$ MPa.

These relations yield

(18a) $-n_1 + 3n_2 = 0$ ($\sigma_1 = 11$ MPa) (18b) $3x_1 + x_2 = 0$ ($\sigma_2 = 1$ MPa). From (18a), for an eigenvalue (principal value) of 11 MPa, $n_1 = 3n_2$. From (18b), for an eigenvalue (principal value) of 1 MPa, $n_2 = -3 n_1$.



For $\sigma_1 = 11MPa^*$

$$\theta_{x1,normal} = \tan^{-1} \left(\frac{x_2 / |\mathbf{n}|}{x_1 / |\mathbf{n}|} \right) = \tan^{-1} \left(\frac{n_2}{n_1} \right) = \tan^{-1} \left(\frac{n_2}{3n_2} \right) = \tan^{-1} \left(\frac{1}{3} \right) = 18.5^{\mathsf{C}}$$

For $\sigma_2 = 1$ Mpa*

$$\theta_{x1,normal} = \tan^{-1} \left(\frac{x_2 / |\mathbf{n}|}{x_1 / |\mathbf{n}|} \right) = \tan^{-1} \left(\frac{n_2}{n_1} \right) = \tan^{-1} \left(\frac{-3n_1}{n_1} \right) = \tan^{-1} \left(-3 \right) = -71.5^{\mathsf{c}}$$

The two eigenvectors are perpendicular, as they are supposed to be.

* In the first expression for θ , the normal direction is the x1' direction, and n1 and n2 are the direction cosines for a unit vector along x1'. In the first expression for θ , the normal direction is the x2' direction, and n1 and n2 are the direction cosines for a unit vector along x2'.

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Matrix treatments of stress transformation V In matrix form, $\sigma_{i'i'} = a_{i'k}a_{i'l}\sigma_{kl}$ becomes (Mal & Singh, 1991, p. 37) (19) $\sigma' = [a] [\sigma] [a^T],$ where (20) $a = \begin{bmatrix} a_{1'1} & a_{1'2} & a_{1'3} \\ a_{2'1} & a_{2'2} & a_{2'3} \\ a_{3'1} & a_{3'2} & a_{3'3} \end{bmatrix}$ and (21) $a^T = \begin{bmatrix} a_{1'1} & a_{2'1} & a_{3'1} \\ a_{1'2} & a_{2'2} & a_{3'2} \\ a_{1'3} & a_{2'3} & a_{3'3} \end{bmatrix}$ The proper order of matrix multiplication is essential in order to reproduce the expansions of lecture 17: [a] $[\sigma] [a^T]_{\neq} [a^T] [\sigma][a]!$ In MATLAB, equation (19) would be written: sigmaprime = a * sigma * a' The term a' signifies [a^T]. Matlab also has a function "eig" to find eigenvectors (given in terms of the direction cosines) and eigenvalues. [V,D] = eig (sigma)Example $sigmaxy = [10 \ 3;3 \ 2]$ sigmaxy = 10 3 3 2 »a = [3/sqrt(10) 1/sqrt(10);-1/sqrt(10) 3/sqrt(10)] a = 0.9487 The first row of matrix "a" is the negative 0.3162 -0.3162 0.9487 of the first column of matrix V below. The second row of matrix "a" is the negative $sigmaprime = a^sigmaxy^a'$ of the second column of matrix V below. sigmaprime = 11.0000 -0.0000 -0.0000 1.0000 [V,D] = eig(sigmaxy)V = -0.9487 0.3162 Column 1 in V relates to column 1 in D Column 2 in V relates to column 2 in D -0.3162 -0.9487 D = 0 11 1 0